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# A Decision Support System for Strategic Maintenance Planning in Offshore Wind Farms

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This paper presents a Decision Support System (DSS) for maintenance cost optimisation at an Offshore Wind Farm (OWF). The DSS is designed for use by multiple stakeholders in the OWF sector with the overall goal of informing maintenance strategy and hence reducing overall lifecycle maintenance costs at the OWF. Two optimisation models underpin the DSS. The first is a deterministic model that is intended for use by stakeholders with access to accurate failure rate data. The second is a stochastic model that is intended for use by stakeholders who have less certainty about failure rates. Solutions of both models are presented using a UK OWF that is in construction as an example. Conclusions as to the value of failure rate data are drawn by comparing the results of the two models. Sensitivity analysis is undertaken with respect to the turbine failure rate frequency and number of turbines at the site, with near linear trends observed for both factors. Finally, overall conclusions are drawn in the context of maintenance planning in the OWF sector.

Key words: offshore wind, renewable energy, Operations and Maintenance (O&M), decision support, stochastic optimisation

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## 1. Introduction

The EU aims to achieve 20% of energy consumption from renewable sources in order to reduce carbon emissions by 2020 (Bilgili *et al.*, 2011; Laura and Vicente, 2014). The UK government has also set the figure of 15% as the target for 2020 (O'Keeffe and Hagett, 2012; Higgins and Foley, 2014). Over the past decade, wind energy has been a significantly developing renewable energy source (Ding and Tian, 2012). According to the interviews conducted by Ochieng *et al.* (2014), wind power is one of the few renewable technologies that demonstrate a rapid development in the past decades. It will therefore provide a major proportion of electricity production out of all the renewable sources (Freris and Infield, 2009) and make a great single contribution to the 2020 target (O'Keeffe and Hagett, 2012; Appiott *et al.*, 2014). There are five distinct phases during the life cycle of an offshore wind farm: development and consenting, production and acquisition, installation and commissioning, operation and maintenance (O&M) and decommissioning (Myhr *et al.*, 2014). The O&M starts when the OWF begins operating and continues until the final decommissioning stage. Although the cost of the O&M phase is generally not as large as the construction phase, it is still significant due to the length of the long-term operation during the life cycle. O&M costs are of the order of £25-40 million for a typical 500MW OWF (The Crown Estate, 2010). These kinds of cost accounts for 18% of the total offshore wind system (Carbon Trust, 2008). Hence the expenditure on O&M may be seen as a key element of the energy production costs in OWFs.

One of the challenges of performing maintenance operations in OWFs is the transport of personnel, spare parts and large components to individual wind turbines by vessels or helicopters (Halvorsen-Weare *et al.*, 2013). Due to the expensive purchase price or charter-in rate, the use of specialised vessels or helicopters can account for a high percentage of the O&M costs. The maintenance activities for an offshore wind project need a fleet of vessels, such as component transport vessels, crew transfer vessels, crane vessels, and vessels for specialised tasks such as cable-laying (Halvorsen-Weare *et al.*, 2013). The type of vessel or helicopter used for maintenance depends significantly on the distance from the port to the OWF (Laura and Vicente, 2014). Vessel efficiency is becoming a key factor in determining overall vessel demand, which is defined in terms of working time required for recovering different faults, taking into account weather delays.

O&M costs are not only caused by repair and replacement of components, but also by production loss due to downtime (Scheu *et al.*, 2012). Maintenance management aims at improving the availability of the production systems and reducing the overall maintenance cost (Ding and Tian, 2012). The revenue loss can be presented by calculating the required time of planned and unplanned service and the productivity level. Minimisation of downtime strongly depends on the accessibility of the installed facilities. Maintenance of any offshore system is not an easy job because of restricted logistics and accessibility.

In order to minimise the expected costs in the lifetime of an OWF, an optimal plan for O&M should be developed in order to handle the component failure risk (Nielsen and Sorensen, 2011). The central question in developing the optimal plan is the decision of when and how to organise maintenance activities. The existing industry experiences imply that production loss might result from the lack of inspection/repair prior to component failure. A survey of offshore wind energy companies was conducted by the work of Pahlke (2007), with 70% of the respondents expressing the need for decision support tools whereas only a few of them had such models available for use (Scheu *et al.*, 2012; Hofmann and Sperstad, 2013). The literature review presented in this paper shows that the developed decision support tools to date use mainly simulation techniques, whilst the use of mathematical optimisation modelling is limited.

The maintenance frequency affects activity demand and costs associated in the operation time of vessels and technicians, especially the corrective maintenance for component

breakdown. The unplanned events for repairs/replacement of failed OWF components account for a high percentage of the maintenance tasks, typically between 50-70% (Van Bussel, 1997). The maintenance practices of OWFs can be optimised with respect to the failure rates and service costs of wind turbines in the marine environment. The development of an optimised maintenance schedule for OWFs could potentially minimise the maintenance expedition costs, through the use of statistical data on offshore wind turbine failure rates (Kooijman *et al.*, 2004).

In this paper, a Decision Support System (DSS) is developed to give multiple stakeholders in offshore wind farms a tool to assist them in making decisions to conduct cost effective maintenance in OWFs. The maintenance operations include selection of maintenance strategies for project developers, identification of the annual number of required technicians for HR managers, and the required chartered vessels for O&M planners, in order to achieve a minimum cost. Deterministic and stochastic optimisation models are proposed to optimise personnel, transport, and breakdown costs of O&M. The deterministic model is used when the failure rate is known, whilst the stochastic model is utilised in case the failure data is unknown from operational practices. The optimisation models and the solution method are integrated into the DSS to build an efficient decision tool for optimising and analysing maintenance activities. The DSS has been developed part of the 2OM (Offshore Operations & Maintenance Mutualisation) project, financed by the EU Interreg IVA France (Channel) – England programme.

The rest of the paper is organised as follows: In Section 2, an overview of existing decision support on offshore wind maintenance is presented. Sections 3 and 4 describe the DSS and the optimisation models for the strategic planning of offshore wind farm maintenance. Experimentation results and sensitivity analysis of the system are demonstrated in Section 5. Finally, some concluding remarks and suggestions for further research are provided in Section 6.

## **2. An overview of decision support tools for offshore wind maintenance**

Computational decision tools are able to support complex decision making in the energy sector, such as the recent tools developed by Hunt *et al.* (2013) and Chang (2014) for the planning and coordination of renewable energy systems. A performance analysis of a renewable energy system usually underpins this kind of tool to aid decision making. Most of the developed decision support systems in the wind energy sector are specific to onshore developments and only a small number of those are suitable for offshore projects (Pahlke, 2007). The tools are more likely applicable offshore in a limited geographical area rather than a large extent such as the North Sea, which contains a large number of current and proposed wind farms from several countries (Wanderer, 2009).

As O&M costs account for around one third of the life cycle cost of an offshore wind farm, there is a need to develop cost-effective O&M strategies to achieve a significant saving in the cost of energy during the life of OWFs. A number of researchers over recent years have created decision support tools for different purposes in offshore wind production, such as to forecast the operations of a wind farm (Scheu *et al.*, 2012), to estimate the O&M costs including revenue loss (Dinwoodie *et al.*, 2013), to assess offshore wind energy potential (Schillings *et al.*, 2012), and to simulate the operational phase of an offshore wind farm with all maintenance activities and costs (Hofmann and Sperstad, 2013). A common objective of these tools is to find the optimal maintenance strategy/planning for a particular offshore wind farm, rather than a global strategy for multiple farms. The decision tools may calculate the maintenance cost on the basis of levelised production cost (LPC), which is seen as an efficient way for analysis and evaluation of risk and total cost during the life span of offshore turbines (Myhr *et al.*, 2014), Dinwoodie *et al.* (2015) investigated the performance amongst

the existing simulation models of operation and maintenance for offshore wind farms; they also identified key model assumptions that impact model results.

The Norwegian offshore wind cost and benefit model – NOWIcob (Hofmann and Sperstad, 2013) can simulate the operational phase of an offshore wind farm with all maintenance activities and costs. Several input parameters, both controllable options and the uncontrollable external factors, can be changed in the model to assess their impact on performance parameters such as the O&M costs and availability. Controllable options are all strategic choices that the wind farm operator can directly decide upon. Uncontrollable external factors include all parameters that are outside the direct influence of the wind farm operator such as the market environment and weather conditions.

Most of the tools concentrate on the modelling of failures and repair, although these two parameters are often assumed to be deterministic. Nevertheless stochastic modelling is suggested to simulate the variability of the failure rates of wind turbine components, since a deterministic approach would not give realistic results. Discrete-event simulation is a powerful computational technique, which has been to solve problems with stochastic data (Willis and Jones, 2008).

Operational research (OR) has a long tradition in improving operations and especially in reducing costs (Dekker *et al.*, 2012). In the renewable energy sector, a range of OR approaches have been applied in production scheduling, transportation routing and maintenance supply planning. For example, Zhang *et al.* (2013) presented an optimisation model for scheduling power generation in a wind farm. Similar works in scheduling and capacity planning of renewable energy have been reviewed by Connolly *et al.* (2010) and Beerbuhl *et al.* (2015). OR techniques have also been used on the optimisation of offshore wind O&M. A mixed integer programming model with binary variables is usually applied to aid decision making in vessel fleet composition problems (Halvorsen-Weare *et al.*, 2013; Hvattum and Nonas, 2013). Vessel properties and contracts should be taken into account to configure the vessel fleet with crews for execution of maintenance operations in OWFs. The most common objective function is to minimise the fixed costs of vessels and ports, variable costs using the vessels, expected downtime costs of delayed correct maintenance activities and penalty and/or transportation costs. The optimal solutions are constrained typically by a limited number of vessels, necessary time spent on a maintenance task, the locations of maintenance resources, and the sea state suitable for carrying out O&M activities.

When modelling O&M practices for OWFs, the reliability of the wind turbines is a key parameter that will affect the output of the project, i.e. energy output and cost per unit of energy produced. However, a lack of publically available offshore wind turbine failure data is a challenge in the decision making of corrective maintenance operations. A number of models have been developed to predict the revenue (Krokozinski, 2003), or to estimate the O&M costs (Van Bussel and Bierbooms, 2003; Obdam *et al.*, 2007) by considering the wind turbine reliability. Reliability models can be utilised to quantify the failure rates of offshore wind turbines and identify the repair time for each type of failure. The energy losses due to wind turbine failures, downtime and maintenance tasks are viewed as an element of maintenance cost. Nevertheless, a significant proportion of failure rates used in previous studies are extracted from onshore wind farm data, and the effect of the marine environment on the offshore wind turbine reliability has not been considered.

From the review of the existing decision support and optimisation models for maintenance in OWFs, there is little research on the integration of optimisation models within the decision support systems. An efficient DSS with user interface for multiple purposes is proposed in this paper, by an integration of decision aiding and optimisation models. The two versions of

the optimisation models, associated with deterministic and stochastic reliability parameters, are formulated on the basis of offshore wind farm O&M practices.

### 3. Description of the DSS for offshore wind O&M

The Decision Support System (DSS) proposed is designed to assist multiple offshore wind stakeholders for determining cost effective maintenance resources for an offshore wind farm. The system can also be used to understand sensitivities of the operation and maintenance costs due to changes in the maintenance and logistics strategy, and to provide an estimate of the maintenance cost. As shown in Figure 1, the DSS requests system and user input data. The tool then identifies the minimum cost to meet the maintenance demand on the basis of the input data. The DSS embeds two optimisation models in order to generate optimal maintenance costs on the resources required to conduct the maintenance. Finally the requirement of maintenance resources, facilities in port and training courses are given as outputs of the system.

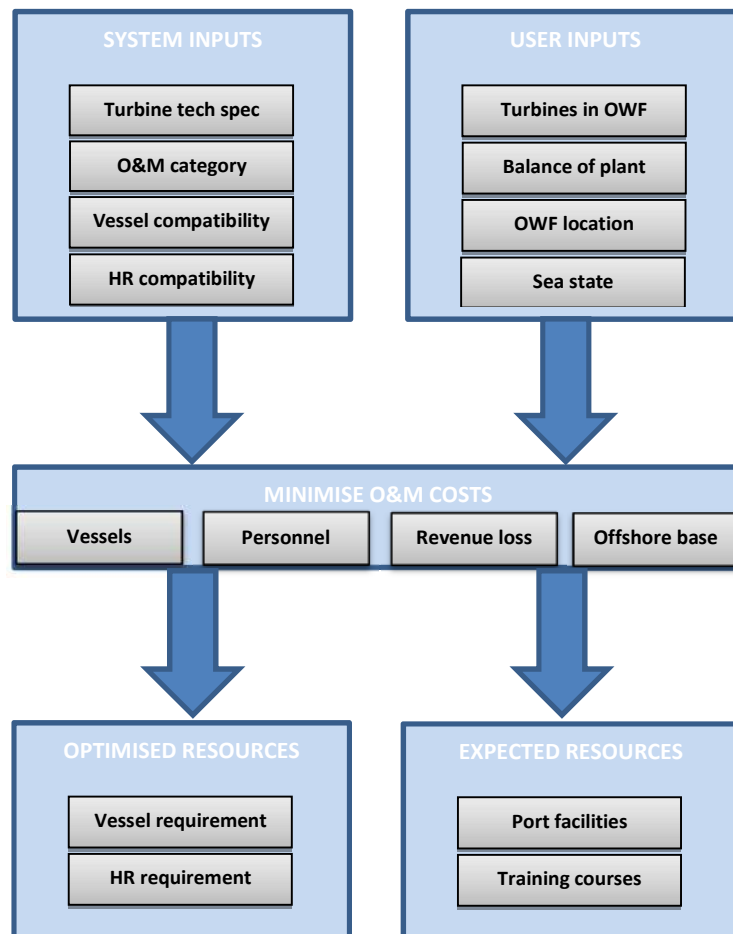


Figure 1: Decision Support System framework

#### 3.1 System inputs

System input data is entered into the DSS prior to users providing the information of a particular project, including the technical specification of existing wind turbines in the current market, characteristics of the pre-defined maintenance categories, and compatibility of vessels and technicians on different maintenance categories. The wind turbine specification is imported from the 4cOffshore website (<http://4cOffshore.com>). Categorisation of maintenance activities and compatibility of vessels and technicians are underpinned by the practical data collected from a wide range of experts in the offshore wind sector.

#### • **Categorisation of maintenance**

In order to design the DSS, expert opinions about O&M in the industry were collected from different stakeholders in the offshore wind sector, such as O&M managers, O&M consultants, technicians, and port managers, by the use of an online survey, interviews and working groups. Further details are available at the 2OM project WP 4: communication (Li *et al.*, 2015). According to the responses from the industry experts, offshore wind maintenance activities are classified into nine categories (see Table 1) in the DSS, four preventive and five corrective categories. The number of vessels and technicians should be identified in order to undertake the different maintenance tasks.

Preventive maintenance (PM):	Corrective maintenance (CM):
Cat. C1: PM on wind turbines	Cat. P1: CM for wind turbine repair
Cat. C2: PM on foundations	Cat. P2: CM for wind turbine minor replacement
Cat. C3: PM on substations	Cat. P3: CM for wind turbine major replacement
Cat. C4: PM on cables	Cat. P4: CM for substation repair / replacement
	Cat. P5: CM for cable repair / replacement

Table 1: Preventive and corrective maintenance categories

For each category, the length of time required for preparation, repair and logistics are determined. The *preparation time* is the duration of mobilisation of all necessary resources. *Repair time* covers the time that the technicians use during repair or replacement. *Logistics time* typically incurs when a turbine component is ordered from the manufacturer. In addition, the size of maintenance crew is also determined depending on the workload of each maintenance category. The main activities in both preventive and corrective maintenance are the transport of the maintenance crew and components and the execution of repair or replacement. The most suitable vessel and the crew with the necessary skills should be selected to execute an inspection or correct a failure according to the compatibility of each vessel and personnel type.

#### • **Compatibility of vessels and technicians (HR)**

A range of vessels can be chartered, on a short-term or/and long-term lease, to carry out maintenance tasks during the planning horizon. Crew transfer vessels are utilised widely in the offshore energy field, such as oil and gas. Crane vessels and jack-up vessels are used to replace wind turbine components, depending on the size of the work. Helicopters can support the transportation of personnel and equipment in emergencies and can reduce the length of downtime. Daughter ships must work with a mother ship offshore; they can offer preventive inspection and corrective repairs on wind turbines. In practice, at most one mother ship may undertake maintenance works for a particular offshore wind farm. The

compatibility of each vessel type varies with the maintenance categories. The length of lease of each type of vessel should cover its requirement for different maintenance categories. Each type of vessel has a given service speed, restricted use due to weather conditions and lease cost.

Currently no single standardisation of maintenance technicians exists in the offshore wind industry. With respect to the personnel data from survey responses, technicians involved in the DSS are classified into four groups in terms of job function and base location.

- Onshore-based turbine technicians are responsible for maintaining the condition of the turbines.
- Offshore-based turbine technicians are considered only if an offshore platform is utilised, such as a mother ship with daughter ships.
- Foundation technicians are in charge of the maintenance work on the turbine foundation.
- Electrical technicians undertake the repair and/or replacement in both substations and cables.

When the personnel are scheduled for offshore maintenance works, the shift length may impact on the efficiency of the activities. In practice, the length of an on-duty shift is seen as a hard constraint to restrict the daily workload.

### **3.2 User inputs**

A graphical friendly user interface provides users with an easy way to use the system, by inputting a series of input variables about OWF(s) and outputting the corresponding O&M resource requirements. The user input variables include data on the turbines, balance of plant, location and sea state, which therefore focus on the technical, structural and environmental information of an offshore wind farm. The input variables for a particular offshore wind project are fed through the system in order to produce for the user a series of O&M resource requirements.

### **3.3 Cost optimisation**

The bulk of the system is comprised of a series of key assumptions, objective functions and constraints that use the data inputs to generate the required maintenance resources at a minimum cost, in particular vessels and technicians. The optimal costs are acquired by the deterministic or stochastic models which are described in detail in Section 4. The objective of the models is to minimise the O&M costs, including the costs of personnel, vessel, and production loss due to downtime. The major constraints considered are the available working time of personnel, capacity, compatibility and weather restriction of each vessel type. The deterministic model is used for the case with known technical failure rates of wind turbine components. Otherwise, the failure frequency is assumed as a probabilistic parameter in the stochastic model.

### **3.4 System outputs**

According to the cost estimation from the DSS, the OWF management team will decide on the most suitable maintenance strategy with respect to some operational issues in practice, e.g. available space and support workers in the maintenance base port. There are three optional maintenance strategies that are defined in the DSS in terms of vessel and personnel resources required; namely *port based*, *port with helicopters* and *offshore based*.



The three optional strategies have distinct requirements for vessels/helicopters, human resources (HR), port facilities, and personnel training courses. The optimised vessels and human resources are determined by the proposed optimisation models to meet the maintenance requirements. Essential port facilities and personnel training courses are suggested by the DSS, such as sufficient storage space and parking space as port facilities; project management and under-water work skills as training programmes.

For a port based strategy, different types of vessels are used to carry out maintenance, which is usual for most of the existing offshore wind farms as the distance to port is not great. In order to minimise the rescue time, helicopters may be considered to assist urgent repairs with a quick response. However, additional facilities are required in the base port, such as a heli-pad and fuel pumps. With such strategies, with or without a helicopter, the majority of the O&M resources are located at the onshore maintenance port, and all vessels and helicopters are assumed to return by the end of each day. With the increased distance between the wind farm and the shore in the new generation offshore wind farms, operators may tend to use offshore based maintenance. In this way, a mother ship with daughter ships may stay offshore for a period of time to reduce the travel distance, compared to other types of vessels. Additional training courses are needed for these offshore based technicians. Such an offshore based platform does not only offer a quicker response for unforeseeable failures, but can also be used in preventive inspections.

## **4. Optimisation models**

To reduce the costs of maintenance activities in an OWF, we propose deterministic and stochastic optimisation models to minimise personnel, vessel, and breakdown costs. These two optimisation models are integrated into the DSS. The deterministic model is intended for use by stakeholders with access to accurate failure rate data. The stochastic model is intended for use by stakeholders who have less certainty about failure rates.

### **4.1 Notation and assumptions**

Index  $k$  denotes the category of maintenance.  $k = 1 \dots 4$ , indicate the preventive maintenance activities;  $k = 5 \dots 9$ , indicate corrective maintenance. Four kinds of maintenance technicians are considered in the model  $i = 1 \dots 4$  represent onshore based turbine technician, foundation technician including underwater maintenance, electrical technician for maintenance of cables and substations, and offshore based turbine technician respectively. A variety of vessels are used to transfer the crew to execute different maintenance tasks, type  $j = 1 \dots 5$  denote crew transfer vessel, crane vessel, jack-up, helicopter and daughter ship (working with a mother ship respectively).

$i \in I$ : Set of technician types  
 $i = 1$ : turbine technicians (onshore based)  
 $i = 2$ : foundation technicians  
 $i = 3$ : electrical technicians  
 $i = 4$ : turbine technicians (offshore based)

$j \in J$ : Set of vessel types  
 $j = 1$ : crew transfer vessels  
 $j = 2$ : crane vessels  
 $j = 3$ : jackups  
 $j = 4$ : helicopters  
 $j = 5$ : daughter ships

358  $k \in K$ : Set of maintenance categories  
 $k = 1$ : preventive maintenance of wind turbines  
 $k = 2$ : preventive maintenance of substations  
 $k = 3$ : preventive maintenance of foundations  
 $k = 4$ : preventive maintenance of cables  
 $k = 5$ : corrective maintenance for wind turbine repair  
 $k = 6$ : corrective maintenance for wind turbine minor replacement  
 $k = 7$ : corrective maintenance for wind turbine major replacement  
 $k = 8$ : corrective maintenance for substation repair/replacement  
 $k = 9$ : corrective maintenance for cable repair/replacement  
 359  
 360  $C_i^P$ : annual salary of technician type  $i$   
 $C_j^F$ : annual fixed cost of vessel type  $j$   
 $C_j^V$ : variable cost per hour of vessel type  $j$   
 $C^M$ : annual charter cost for mothership  
 $R^L$ : revenue loss per hour  
 361  $d_j$ : distance to shore for vessel  $j$   
 $s_j^V$ : average speed of vessel type  $j$   
 $F_k$ : annual maintenance frequency of category  $k$   
 $H_i^P$ : number of working hours for technician type  $i$  in one day  
 $H_j^V$ : number of working hours for vessel type  $j$  in one day  
 $L_i^P$ : annual number of available working days for technician  $i$   
 $L_j^V$ : annual number of available working days for vessel  $j$   
 362  
 $L_k^{Repair}$ : length of maintenance (repair) time for category  $k$   
 $L_k^{logistics}$ : length of logistics time for category  $k$   
 $L_j^{Prepare}$ : length of preparation time for vessel  $j$   
 $L_j^{Travel}$ : length of travel time from shore to offshore wind farm for vessel  $j$   
 363  $q_k$ : number of technicians required for maintenance category  $k$   
 364  $Q_j$ : the capacity of vessel  $j$  to carry technicians  
 $U_k$ : the number of maintenance unit for  $k$   
 $N$ : the number of turbines  
 $V^{daughter}$ : maximum number of daughter ships carried by a mother ship  
 $r^{Array}$ : the average length of array cable required for a wind turbine  
 $r^{Sub}$ : the average number of wind turbines connected by a substation  
 365  
 $Z_{ik}^P \begin{cases} 1: \text{technician } i \text{ is compatible to execute maintenance } k \\ 0: \text{technician } i \text{ is not compatible to execute maintenance } k \end{cases}$   
 $Z_{jk}^V \begin{cases} 1: \text{vessel } j \text{ is compatible to execute maintenance } k \\ 0: \text{vessel } j \text{ is not compatible to execute maintenance } k \end{cases}$   
 366  
 367 **Decision variables:**  
 $x_{ik}$ : number of required technicians type  $i$  for maintenance  $k$   
 $X_i$ : annual number of technicians type  $i$   
 368  
 $y_{jk}$ : number of required vessel type  $j$  used for maintenance  $k$   
 $Y_j$ : annual number of vessel  $j$   
 369  
 $b_{ik}^P \begin{cases} 1: \text{if technician type } i \text{ is used to execute maintenance } k \\ 0: \text{otherwise} \end{cases}$   
 370

$b_{jk}^V \begin{cases} 1: \text{if vessel type } j \text{ is used to execute maintenance } k \\ 0: \text{otherwise} \end{cases}$

$b^M \begin{cases} 1: \text{a mother ship is used} \\ 0: \text{otherwise} \end{cases}$

As personnel in the model are assumed to be full-time workers, the personnel cost is estimated using the annual salary ( $C_i^P$ ) of each technician type  $i$ . There are two costs considered for vessels: fixed cost of charter ( $C_j^F$ ) per vessel of type  $j$  and a variable cost ( $C_j^V$ ) in respect to the hours that a vessel is used in maintenance. The fixed cost is a charge incurred at the beginning of an annual or monthly lease. A mother ship is usually required when daughter ships stay offshore for maintenance activities, so a separate cost is considered for the charter of a mother ship ( $C^M$ ). Downtime due to maintenance service execution also contributes a significant portion of the maintenance cost. It is referred as revenue loss in terms of the hourly rate of production income ( $R^L$ ) and length of downtime. All turbines in a given offshore wind farm are assumed homogenous with respect to manufacture model and production capacity.

Travel time ( $L_j^{Travel}$ ) for vessel type  $j$  is calculated by the distance ( $d_j$ ) and its speed ( $s_j^V$ ). The preparation time of a vessel ( $L_j^{Prepare}$ ) depends on the vessel type  $j$ , while the repair/replacement time ( $L_k^{Repair}$ ) and logistics time ( $L_k^{Logistics}$ ) are pre-determined by the category of maintenance  $k$ . All the above timing data are constants in the model.

Weather conditions give a safety restriction at which a vessel type can operate at wind turbines, in terms of wave height and wind speed. If the weather conditions reach one of the operational limits of the vessel, the maintenance activities will be postponed. As DSS supports strategic decisions on optimal maintenance resources, it is not a tool that determines the daily maintenance activities with respect to weather conditions. The parameter ( $L_j^V$ ) is used to represent the number of available days that vessel type  $j$  can undertake maintenance tasks. Another parameter, the number of available days for technicians  $i$  ( $L_i^P$ ), would be restricted by the use of vessels. The number of working hours in each day for vessels ( $H_j^V$ ) and technicians ( $H_i^P$ ) are equal, which should be a key operation constraint to restrict the daily workload.

A maintenance team is usually sent to execute an inspection or repair; the number of technicians ( $q_k$ ) in such a team depends on the work size of maintenance category  $k$ . Each maintenance category requires compatible technicians and vessels in action. For instance, a major replacement of large turbine components must be executed by a jack-up vessel, rather than small or medium size vessels. The compatibility of each technician and vessel type is represented by the binary data  $Z_{ik}^P$  and  $Z_{jk}^V$ . The binary data taking the value 1 indicates that the given type of technician or vessel is compatible to work for the specific maintenance categories, otherwise it takes the value 0. According to the data acquired from O&M specialists in the sector, the two binary data sets, compatibility of technicians  $i$  and vessels  $j$  for maintenance category  $k$ , are clarified in Tables 2 and 3.

$Z_{ik}$	1	2	3	4	5	6	7	8	9
1	1	0	0	0	1	1	1	0	0
2	0	0	1	0	0	0	0	0	0
3	0	1	0	1	0	0	0	1	1
4	1	0	0	0	1	1	1	0	0

Table 2: Compatibility of each technician type

$Z_{jk}$	1	2	3	4	5	6	7	8	9
1	1	1	1	1	1	0	0	1	1
2	0	0	0	0	0	1	0	0	0
3	0	0	0	0	0	0	1	0	0
4	0	0	0	0	1	0	0	1	0
5	1	0	0	0	1	0	0	0	0

Table 3: Compatibility of each vessel type

A daughter ship ( $j = 5$ ) travels for a short distance and time at sea. All other types of vessels ( $j = 1 \dots 4$ ) must depart from the onshore maintenance port. The optimisation model takes into account the maintenance operations of one offshore wind farm. The model does not consider the vessel routes for implementing the maintenance activities. The travel distance of a vessel departing from an onshore port or a mother ship will take the average level value, to all wind turbines in an offshore wind farm.

## 4.2 Deterministic optimisation model

The deterministic optimisation model is formulated and used for the case with known technical failure rate of wind turbine components. This model is designed, as an option, in the DSS for users who know the failure rates of OWF components; so the frequency of each maintenance category is recognised to be deterministic input data.

### 4.2.1 Objective function

The objective function consists of minimising the total amount of the five different costs that occur when executing all the maintenance activities at an OWF during a given period (e.g. one year). The total cost contains personnel cost, fixed and variable costs of vessels, mother ship cost and downtime cost that is the revenue loss while a wind turbine is failed or under inspection.

*Total O&M cost*

$$= \text{Personnel cost} + \text{Vessel fixed cost} + \text{Vessel variable cost} \\ + \text{Mothership cost} + \text{Downtime cost}$$

A maintenance unit ( $U_k$ ) is defined according to the maintenance categories and the components in an offshore wind farm. For instance, a maintenance unit for category 1 (preventive maintenance on wind turbines) is one wind turbine; while a maintenance unit for category 2 (preventive maintenance on substations) represents a substation. An average number of wind turbines connected to a substation is defined as a rate ( $r^{Sub}$ ). A maintenance unit of cable implies 100km. Array cable is estimated in respect to the average length of cable required on each turbine ( $r^{Array}$ ), and length of an export cable is approximated by the distance to shore and number of the substations.

$$U_k = N \quad k = 1,3,5,6,7 \quad (1a)$$

$$U_k = N / r^{Sub} \quad k = 2,8 \quad (1b)$$

$$U_k = (N \cdot r^{Array} + D \cdot N / r^{Sub}) / 100 \quad k = 4,9 \quad (1c)$$

- Annual personnel cost

Total personnel cost is determined by the annual salary ( $C_i^P$ ) and the number of full-time technicians employed ( $X_i$ ) in each type  $i$ .

$$Personnel\ cost = \sum_{i \in I} C_i^P \cdot X_i \quad \forall i \in I$$

(2a)

• Vessel fixed cost

The fixed cost of vessel of type  $j$  is determined in terms of the charter rate ( $C_j^F$ ) per lease period (e.g. a year or a repair event). Crew transfer vessels, helicopters and daughter ships are assumed to be chartered annually, so the number of such vessel types ( $Y_j$ ) are critical to estimate the total fixed cost. Crane vessels and jack-up vessels are usually chartered monthly at events that a major repair or a replacement is required.

$$vessel\ fixed\ cost = \sum_{j \in J} C_j^F \cdot Y_j \quad \forall j \in J$$

(2b)

• Vessel variable cost

The variable cost rate is hourly ( $C_j^V$ ) for each type of vessels. The travel time of vessel  $j$  from maintenance port to offshore wind farm is defined ( $L_j^{Travel} = \frac{d_j}{s_j^V}$ ) by the travel distance over the vessel speed. The actual length of travel time for each maintenance task is usually made up by a returned trip ( $2L_j^{Travel}$ ). The travel time and the length of time required for repair/replacement on the maintenance category ( $L_k^{Repair}$ ) are the two major elements to determine the length of required time of vessel  $j$ .

$$Vessel\ variable\ cost = \sum_{j \in J} \sum_{k \in K} C_j^V \cdot b_{jk}^V \cdot (L_k^{Repair} + 2L_j^{Travel}) \cdot U_k \cdot F_k$$

(2c)

where  $b_{jk}^V$  is a binary variable indicating whether vessel type  $j$  is selected for maintenance  $k$  or not.

• Mother ship cost

The charter expenditure ( $C^M$ ) of a mother ship must be accounted in the O&M cost when a daughter ship is used to undertake maintenance works. So the cost of leasing a mother ship relies on whether or not offshore based maintenance is executed ( $b^M = 0$  or  $1$ ).

$$Mother\ ship\ cost = C^M \cdot b^M$$

(2d)

• Downtime cost

Any revenue loss due to breakdown of turbines or balance of plant is identified as downtime cost, which is constructed by the hourly rate of potential production income ( $R^L$ ) and length of downtime for each period ( $l_t^D$ ). The length of downtime contains preparation time ( $L_j^{Prepare}$ ) and a single trip travel time ( $L_j^{Travel}$ ) of the vessel  $j$  selected, and repair time ( $L_k^{Repair}$ ) and logistics time ( $L_k^{Logistics}$ ) of each maintenance category  $k$ .

- Vessel preparation time ( $L_j^{Prepare}$ ) is a constant, which depends on the vessel type.

- The length of repair/replacement time ( $L_k^{Repair}$ ) is given as a constant of the maintenance category  $k$ . It is not related to the type of vessels or technicians used.
- Similar as the repair time, logistics time ( $L_k^{Logistics}$ ) is another constant parameter associated with each maintenance category.

Hence, the total downtime cost is evaluated by:

$$Downtime\ cost = R^L \cdot l^{Downtime} \quad (2e)$$

Where

$$l^{Downtime} = \sum_{k \in K} \left( \sum_{j \in J} (L_j^{Travel} + L_j^{Prepare}) \cdot b_{jk}^V + L_k^{Repair} + L_k^{Logistics} \right) \cdot U_k \cdot F_k \quad (2f)$$

The objective of the deterministic model is to minimise the sum of the five costs ( $z_d$ ).

$$\begin{aligned} Min\ z_d = & \sum_{i \in I} C_i^P \cdot X_i + \sum_{j \in J} C_j^F \cdot Y_j + \sum_{j \in J} \sum_{k \in K} C_j^V \cdot b_{jk}^V \cdot (L_k^{Repair} + 2L_j^{Travel}) \cdot U_k \cdot F_k \\ & + C^M \cdot b^M + R^L \cdot \sum_{k \in K} \left( \sum_{j \in J} (L_j^{Travel} + L_j^{Prepare}) \cdot b_{jk}^V + L_k^{Repair} + L_k^{Logistics} \right) \cdot U_k \cdot F_k \end{aligned} \quad (3)$$

#### 4.2.2 Constraints

A variety of constraints for the use of vessels and technicians are taken into account in the strategic maintenance planning.

**Constraint set 1:** The working time of compatible technicians should cover the related repair/replacement of a maintenance category  $k$ .

$$x_{ik} \cdot H_i^P \cdot L_i^P \geq q_k \cdot L_k^{Repair} \cdot F_k \cdot U_k \cdot b_{ik}^P \quad \forall i \in I, k \in K \quad (4)$$

**Constraint set 2:** The total working time of each technician type must be larger than the length of time required to undertake all related maintenance.

$$X_i \cdot H_i^P \cdot L_i^P \geq \sum_{k \in K} q_k \cdot L_k^{Repair} \cdot F_k \cdot U_k \cdot b_{ik}^P \quad \forall i \in I, k \in K \quad (5)$$

**Constraint set 3:** As vessels are used to transport technician team(s), and may stay in the offshore wind farm during the maintenance execution for reasons of personnel safety and security, the available time of the selected vessel(s) should cover the time of a 2-way travel and the related repair/replacement of maintenance category  $k$ .

$$y_{jk} \cdot (H_j^V - 2L_j^{Travel}) \cdot L_j^V \geq L_k^{Repair} \cdot F_k \cdot U_k \cdot b_{jk}^V \quad \forall j \in J, k \in K \quad (6)$$

**Constraint set 4:** The total available time of each vessel type must be larger than the length of time required for undertaking all related maintenance.

$$Y_j \cdot (H_j^V - 2L_j^{Travel}) \cdot L_j^V \geq \sum_{k \in K} L_k^{Repair} \cdot F_k \cdot U_k \cdot b_{jk}^V \quad \forall j \in J \quad (7)$$

*Constraint set 5:* The number of technicians transported by all vessels used for maintenance  $k$  is restricted by the overall maximum capacity of the vessels.

$$\sum_{i \in I} x_{ik} \leq \sum_{j \in J} y_{jk} \cdot Q_j \quad \forall k \in K \quad (8)$$

*Constraint set 6:* The number of technicians of type  $i$  used for all maintenance categories  $k$  must be less than the number of technicians of type  $i$  recruited.

$$x_{ik} \leq X_i \quad \forall i \in I, k \in K \quad (9)$$

*Constraint set 7:* The number of vessels of type  $j$  used for all maintenance categories  $k$  must be less than the number of vessels of type  $j$  chartered.

$$y_{jk} \leq Y_j \quad \forall j \in J, k \in K \quad (10)$$

*Constraint set 8:* Technician type  $i$  can be used for maintenance category  $k$  only if the vessel is compatible with the maintenance category.

$$x_{ik} \leq M \cdot Z_{ik}^P \quad \forall i \in I, k \in K \quad (11)$$

where  $M$  is an arbitrarily large positive number

*Constraint set 9:* Vessel type  $j$  can be used to execute maintenance category  $k$  only if the vessel type is compatible to the maintenance category

$$y_{jk} \leq M \cdot Z_{jk}^V \quad \forall j \in J, k \in K \quad (12)$$

where  $M$  is an arbitrarily large positive number

*Constraint set 10:* A binary decision variable is defined to indicate whether technician type  $i$  is selected to execute maintenance category  $k$ .

$$x_{ik} \leq M \cdot b_{ik}^P \quad \text{and} \quad x_{ik} \geq b_{ik}^P \quad \forall i \in I, k \in K \quad (13)$$

*Constraint set 11:* Each maintenance category  $k$  must be served by at least one type of technician.

$$\sum_{i \in I} b_{ik}^P \geq 1 \quad \forall k \in K \quad (14)$$

*Constraint set 12:* A binary decision variable is defined to indicate whether vessel type  $j$  is selected to execute maintenance category  $k$ .

$$y_{jk} \leq M \cdot b_{jk}^V \quad \text{and} \quad y_{jk} \geq b_{jk}^V \quad \forall j \in J, k \in K \quad (15)$$

*Constraint set 13:* Each maintenance category  $k$  must be served by at least one type of vessel.

$$\sum_{j \in J} b_{jk}^V \geq 1 \quad \forall k \in K \quad (16)$$

*Constraint set 14:* The number of each type of technicians must be at least the number required to carry the associated maintenance works.

$$x_{ik} \geq q_k \cdot b_{ik}^P \quad \forall i \in I, k \in K \quad (17)$$

$$X_i \geq q_k \cdot b_{ik}^P \quad \forall i \in I, k \in K \quad (18)$$

*Constraint set 15:* A mother ship will be used ( $b^M = 1$ ) if any daughter ship ( $j = 5$ ) is organised to undertake maintenance jobs.

$$b^M \geq b_{jk}^V \quad j = 5, \quad \forall k \in K \quad (19)$$

*Constraint set 16:* Offshore based turbine technicians ( $i=4$ ) must be transported by the daughter ships ( $j=5$ ) with use of a mother ship for maintenance  $k$ .

$$b_{ik}^P = b_{jk}^V \quad i = 4, \quad j = 5, \quad \forall k \in K \quad (20)$$

*Constraint set 17:* The number of daughter ships used is restricted by the maximum parking space of a mother ship.

$$Y_j \leq V^{daughter} \quad j = 5 \quad (21)$$

### 4.3 Stochastic optimisation model

The second optimisation model in the DSS treats the failure rates of OWF components as a stochastic parameter. This stochastic programming model is integrated into the system for users who provide frequency of each maintenance category as probabilistic scenarios. The advantage of stochastic programming is that it attempts to identify a solution to an optimisation problem while directly addressing uncertainty.

There are three major approaches to stochastic programming, namely probabilistic or chance constraint, modelling future response or resource, and scenario-based analysis (Novak and Ragsdale, 2003). To avoid non-convex constraints and calculation of the resource function with multi-dimensional integration, a range of scenarios of the failure rate for corrective maintenance will be implemented as an effective way to achieve the cost optimisation. A number of additional parameters and decision variables are defined for the failure rate with probability in a set of scenarios.



602  $w \in W$ : Set of scenarios (1...243 in the model)

603

$F_{ks}$ : failure rate of category  $k$  in scenario  $s$

$Pro_{ks}$ : probability of failure rate of category  $k$  in scenario  $s$

$JF_{kw}$ : failure rates for category  $k$  in joint scenario  $w$

$JPro_{kw}$ : probability of failure rate of category  $k$  in joint scenario  $w$

$TPro_w$ : total probability of joint scenario  $w$

604  $TPro_w = JPro_{1w} * JPro_{2w} * \dots * JPro_{kw}$

605 To simulate the variance of corrective maintenance frequency in the stochastic model, failure  
 606 rates of all OWF components are provided by a set of scenarios of probabilistic data. As  
 607 shown by Table 4, each of the five categories is given by three optional levels of failure rate:  
 608 low, mid and high. A corresponding probability of occurrence is associated with each single  
 609 scenario. The mean values of failure rates used in the stochastic model are the same as the  
 610 ones used in the deterministic model.

$k$	$F_{ks}$			$Pro_{ks}$		
	<i>Low</i>	<i>Mid</i>	<i>High</i>	<i>Low</i>	<i>Mid</i>	<i>High</i>
1	1.920	4.275	7.125	0.25	0.50	0.25
2	0.020	0.040	0.120	0.15	0.70	0.15
3	0.030	0.080	0.240	0.15	0.70	0.15
4	1.008	2.250	3.750	0.25	0.50	0.25
5	0.110	0.320	0.960	0.25	0.50	0.25

611 Table 4: Probability distribution of maintenance frequency for category  $k$  in scenarios

612 In respect to the five corrective maintenance categories in Table 4, 243 joint scenarios ( $3^5$ )  
 613 would be considered to predict the maintenance requirements. For instance, the failure rates  
 614 of the maintenance categories  $k$  in joint scenarios 1 ( $JF_{k1}$ ) is (1.092, 0.020, 0.030, 1.008,  
 615 0.110). The associated joint probability in joint scenarios 1 ( $JPro_{k1}$ ) is (0.25, 0.15, 0.15, 0.25,  
 616 0.25). Then by using the equation the total probability ( $TPro_1$ ) is  $0.25 * 0.15 * 0.15 * 0.25 *$   
 617  $0.25 = 0.0003515625$ .

618 The total personnel cost and fixed vessel cost are expressed in the same way as in the  
 619 deterministic model, which consists of optimising the number of each type of technician and  
 620 each type of vessel. Vessel variable cost, mother ship cost and downtime cost are  
 621 determined in terms of the joint scenarios associated with the stochastic combination of  
 622 failure rates in the five corrective maintenance categories. The objective function considers  
 623 the mean cost of vessel variable cost, mother ship cost and downtime cost are considered in  
 624 the objective function, with respect to the different failure rates.

$$\begin{aligned}
 Min \ z_s = & \sum_{i \in I} C_i^P \cdot X_i + \sum_{j \in J} C_j^F \cdot Y_j \\
 & + \sum_{j \in J} \sum_{k \in K} \sum_{w \in W} C_j^V \cdot b_{jk}^V \cdot (L_k^{Repair} + 2L_j^{Travel}) \cdot U_k \cdot JF_{kw} \cdot TPro_w + \sum_{w \in W} C^M \cdot b_w^M \cdot TPro_w \\
 & + \sum_{k \in K} \sum_{w \in W} R^L \cdot \left( \sum_{j \in J} (L_j^{Travel} + L_j^{Prepare}) \cdot b_{jkw}^V + L_k^{Repair} + L_k^{Logistics} \right) \cdot U_k \cdot JF_{kw} \cdot TPro_w
 \end{aligned}
 \tag{22}$$

625

626

627 Subject to

$$x_{ikw} \cdot H_i^P \cdot L_i^P \geq q_k \cdot L_k^{Repair} \cdot F_{kw} \cdot U_k \cdot b_{ikw}^P \quad \forall i \in I, k \in K, w \in W \quad (23)$$

$$X_{iw} \cdot H_i^P \cdot L_i^P \geq \sum_{k \in K} q_k \cdot L_k^{Repair} \cdot F_{kw} \cdot U_k \cdot b_{ikw}^P \quad \forall i \in I, w \in W \quad (24)$$

$$y_{jkw} \cdot (H_j^V - 2L_j^{Travel}) \cdot L_j^V \geq L_k^{Repair} \cdot F_{kw} \cdot U_k \cdot b_{jkw}^V \quad \forall j \in J, k \in K, w \in W \quad (25)$$

$$Y_{jw} \cdot (H_j^V - 2L_j^{Travel}) \cdot L_j^V \geq \sum_{k \in K} L_k^{Repair} \cdot F_{kw} \cdot U_k \cdot b_{jkw}^V \quad \forall j \in J, w \in W \quad (26)$$

$$\sum_{i \in I} x_{ikw} \leq \sum_{j \in J} y_{jkw} \cdot Q_j \quad \forall k \in K, w \in W \quad (27)$$

$$x_{ikw} \leq X_{iw}, X_i = X_{iw} \cdot TPro_w \quad \forall i \in I, k \in K, w \in W \quad (28)$$

$$y_{jkw} \leq Y_{jw}, Y_j = Y_{jw} \cdot TPro_w \quad \forall j \in J, k \in K, w \in W \quad (29)$$

$$x_{ikw} \leq M \cdot Z_{ik}^P \quad \forall i \in I, k \in K, w \in W \quad (30)$$

$$y_{jkw} \leq M \cdot Z_{jk}^V \quad \forall j \in J, k \in K, w \in W \quad (31)$$

$$x_{ikw} \leq M \cdot b_{ikw}^P \text{ and } x_{ikw} \geq b_{ikw}^P \quad \forall i \in I, k \in K, w \in W \quad (32)$$

$$\sum_{i \in I} b_{ikw}^P \geq 1 \quad k \in K, w \in W \quad (33)$$

$$y_{jkw} \leq M \cdot b_{jkw}^V \text{ and } y_{jkw} \geq b_{jkw}^V \quad \forall j \in J, k \in K, w \in W \quad (34)$$

$$\sum_{j \in J} b_{jkw}^V \geq 1 \quad k \in K, w \in W \quad (35)$$

$$x_{ikw} \geq q_k \cdot b_{ikw}^P \quad \forall i \in I, k \in K, w \in W \quad (36)$$

$$X_{iw} \geq q_k \cdot b_{ikw}^P \quad \forall i \in I, k \in K, w \in W \quad (37)$$

$$b_w^M \geq b_{jkw}^V \quad j = 5, \forall k \in K, w \in W \quad (38)$$

$$b_{ikw}^P = b_{jkw}^V \quad i = 4, j = 5, \forall k \in K, w \in W \quad (39)$$

$$Y_{jw} \leq V^{daughter} \quad j = 5 \quad \forall w \in W \quad (40)$$

629

630

631 Sufficient technicians and vessels should be used to meet the maintenance requirement  
 632 ( $F_{kw} \cdot U_k$ ) in each joint scenario  $w$  (Eq.23 - Eq.26). Vessel capacity to carry technicians ( $Q_j$ )  
 633 is still a key constraint here (Eq.27). The number of all technicians for maintenance  $k$  in joint  
 634 scenario  $w$  ( $\sum_{i \in I} x_{ikw}$ ) who are transported by a compatible vessel  $j$  is restricted by the  
 635 vessel's maximum capacity ( $\sum_{j \in J} y_{jkw} \cdot Q_j$ ). Vessel  $j$  or technician  $i$  can be selected to  
 636 execute maintenance  $k$  in joint scenario  $w$  only if the vessel or technician is compatible to the  
 637 maintenance category (Eq.30 and Eq.31). The mother ship contributes a separate vessel  
 638 cost (Eq.38), which is incurred ( $b_{4kw}^P = b_{5kw}^V = 1$ ) if at least one daughter ship ( $y_k^V$ ) is used  
 639 with offshore based technicians ( $x_k^P$ ) in a joint scenario  $w$ .

640

## **5. Implementation and experimental results**

The DSS is implemented on Visual Basic for Application (VBA) as a user interface. The optimisation models, deterministic and stochastic, have been implemented in Xpress, and integrated in the DSS. VBA provides a platform with a high degree of flexibility and control, for constructing the user interface. It also gives the ability to simply import/export data from/to an external database (Agilent Technologies, 2007). Xpress is used to search the optimal solution(s) based on the input data for a particular offshore wind farm. An execution of the DSS using a sample case is described in this section, which will detail the input data and output results. The sensitivity of the DSS is also tested by changing the failure rates and size of OWF.

### **5.1 System input data collection**

The essential system input data of the DSS was collected using an online survey, which was completed by different offshore wind stakeholders. Twenty-nine experts in the sector gave responses to the online survey, including O&M managers, O&M consultants, engineering technicians, and port managers. Further details of the online survey and responses are available on the 2OM project WP1: Maintenance Decision Support Tool (Li *et al*, 2015a). Following on from the survey, a number of interviews to key experts in the industry (including O&M managers and port managers), were arranged in order to acquire further practical information of O&M and to validate the DSS and receive constructive feedback on how the DSS could be improved. In addition, working groups with specialists from the sector was another efficient way to understand the operational issues in offshore wind maintenance. All collected data has been filtered and aggregated, and then entered into the DSS as the system inputs.

Characteristics of the nine maintenance categories are pre-defined in the system, including preparation time, repair/replacement time, logistics time and number of technicians required for each maintenance category. The categorisation of preventive (scheduled) and corrective (unscheduled) maintenance is described in section 3. For the technical specification of wind turbines, such as rated capacity and rated wind speed, they are available from the 4cOffshore website ([http:// 4cOffshore.com](http://4cOffshore.com)).

The VBA-based user interface allows users to modify the parameters and save the settings in the system input data. The saved information can be loaded to the memory for running the system. The user-defined settings are transferred to the software to make decisions for the particular wind farm.

### **5.2 Sample case**

In order to evaluate the proficiency of DSS an implementation with sample data has been carried out. A user input data form has been created with a series of questions to ask the user for the technical, structural and environmental information for an offshore wind farm. The input information is comprised of wind turbines, balance of plant, location and sea state (see Figure 2). The data of Rampion offshore wind farm is used for the user inputs as a sample. Rampion wind farm was a case study for the 2OM (Offshore Operations & Maintenance Mutualisation) project, financed by the EU Interreg IVA France (Channel) – England programme, so the proposed models have been tested on estimated data from the Rampion wind farm since the site (in common with other similar round 3 UK sites) has not yet been built. Rampion offshore wind farm is off the South Coast of the UK, and it is one of

the new ‘round 3’ sites designated by the UK government. 116 wind turbines are currently planned to be installed at the farm, which are specified technically by the rated capacity of 3.45MW and the rated wind speed of 12.5m/s. The average distance from onshore to the farm is 16.9km and the water depth range is between 19 and 39m. Monopile foundations are used to give each wind turbine a total height of 140m. Two 23-km export cables and 140km array cables will be installed. The mean wind speed over the last 10 years is 10m/s.

**Offshore Wind Farm Information**

**Turbine**

Turbine model  
Vestas V112-3.45

Number of turbines  
116

Turbine rated capacity  
3.45 MW

Installed capacity  
400.2 MW

Cut-in wind speed  
3 m/s

Rated wind speed  
12 m/s

Cut-out wind  
25 m/s

**Balance of plant**

Foundation type  
Monopiles

No. of substations  
2

No. of export cables  
2

Array cable length  
140 KM

**Location**

Distance to port  
16.9 miles

Water depth  
19 to 39 m

**Turbine specification**

**Maintenance classification**

Reset

Next

Figure 2: User input data form

Figure 3 shows the information about costs and capacity of each vessel type. The cost and working time of maintenance technicians are also presented in the same data input form of the DSS. All types of vessels except the helicopters are selected in the case study, by clicking the selection boxes, to undertake maintenance works. All personnel types are selected to take part in the maintenance planning.

**Vessel**

Please select	Vessel type	Fixed cost (GBP/year)	Variable cost (GBP/hour)	Speed (miles/h)	Personnel space
<input checked="" type="checkbox"/>	Crew transfer vessel	182500	30	40	12
<input checked="" type="checkbox"/>	Crane vessel	90000	2000	25	12
<input checked="" type="checkbox"/>	Jack-up vessel	102000	1600	20	12
<input type="checkbox"/>	Helicopter	875000	1000	220	3
<input checked="" type="checkbox"/>	Daughter ship	0	120	30	3
<input checked="" type="checkbox"/>	Mother ship	6570000	0	0	12

**Personnel**

Please select	Personnel type	Annual salary (GBP)	Work shift (hour)	Work day (days/year)
<input checked="" type="checkbox"/>	Turbine technician (onshore)	48000	10	180
<input checked="" type="checkbox"/>	Foundation technician	45000	10	180
<input checked="" type="checkbox"/>	Electrical technician	48000	10	180
<input checked="" type="checkbox"/>	Turbine technician (offshore)	58000	12	180

**Wholesale price of electricity**  
1.5 GBP / GW

Back

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Figure 3: System input data form of vessels and technicians

Maintenance frequency for both preventive and corrective activities, as the critical parameters to identify the workloads, must be supplied at the next stage (see Figure 4). For preventive maintenance, the frequency indicates how often the user plans to conduct an inspection / repair on each OWF component. Similar data for the corrective maintenance depends significantly on the component failure rates. Two options of mathematical models, namely deterministic or stochastic, are implemented in the DSS to generate solutions with minimum cost. In case users can just supply the mean value of maintenance frequency, they need to give the data in the 'mean frequency' column and choose deterministic optimisation. The users who have probabilistic maintenance frequencies for each corrective category can input multiple level frequency data with the incurrence probabilities. The user can then select the stochastic optimisation model in order for the DSS to take into account the various levels of frequencies and provide more realistic solutions. Figure 4 illustrates the frequency of both preventive and corrective maintenance. The stochastic model is used to optimise the maintenance planning by giving the probabilistic data at low, mean and high levels.

**Preventive maintenance** | Corrective maintenance

Maintenance category	Maintenance frequency
P1: Inspection / repair on turbines	1
P2: Inspection / repair on substations	1
P3: Inspection / repair on foundations	0.5
P4: Inspection / repair on cables	0.25

**Preventive maintenance** | **Corrective maintenance**

Maintenance category	Low frequency	Mean frequency	High frequency
C1: Repair on turbines	1.920	4.275	7.125
C2: Replacement of minor parts (<2000kg)	0.020	0.040	0.120
C3: Replacement of minor parts (>2000kg)	0.030	0.080	0.240
C4: Repair/replacement on substations	0.008	0.250	0.750
C5: Repair/replacement on cables	0.110	0.320	0.960

Go to deterministic optimisation | Go to stochastic optimisation

Figure 4: Maintenance frequency inputs

In this study, the deterministic and stochastic models were coded and solved using Xpress IVE software on a work laptop with Corei5 2.8gigahertz and 4gigabytes RAM. All optimal solutions in respect to different input data were acquired within a reasonable range of implementation time. With regards to the expected maintenance workload, the DSS computes the number of hours of use of each vessel type and technicians in different maintenance categories. All the results are determined by the optimisation models in order to meet the demand. As the results show in Figure 5, no offshore-based vessel and technician, including mother ships, daughter ships and offshore-based turbine technicians, are used in this plan although they are clicked as available maintenance resources. The offshore based maintenance strategy does not give an obvious advantage at a relatively short distance (16.9km) from the OWF to shore. The majority of the personnel working hours on both preventive and corrective maintenance are also found in the onshore-based turbine technician teams, which is consistent with the usage of maintenance vessels. Figure 5 shows that crew transfer vessels (CTVs) are assigned to all of the preventive maintenance (530 hours) and most of the corrective maintenance (4529 hours). Crane vessels and jack-

up vessels are responsible for replacement of components in corrective maintenance. Since the helicopter was not selected in the input data, no work hours are allocated to it.

By comparing the maintenance hours between preventive and corrective tasks, 91% of the vessel hours and 77% of personnel hours are spent on corrective maintenance, which implies that the reliability of turbine components influences significantly the requirement of maintenance resources. Therefore it is important to determine a trade-off between the amount of preventive and corrective maintenance to reduce cost of corrective maintenance activities. Additionally, the essential operation facilities in a maintenance base port and the qualification training courses for different technical level or administrative personnel are also recognised to match the requirement of O&M activities, in a separate output form.

Preventive Maintenance (scheduled)									
Maintenance category	Vessel time requirement (Hour)					Crew time requirement (Hour)			
	CTVs	Crane vessels	Jack-up vessels	Helicopters	Daughter ships	On. Tur	Foundation	Electrical	Off. Tur
Cat. P1: Inspection / repair on turbines	330	0	0	0	0	1856	0	0	0
Cat. P2: Inspection / repair on substations	6	0	0	0	0	0	0	48	0
Cat. P3: Inspection / repair on foundations	165	0	0	0	0	0	1392	0	0
Cat. P4: Inspection / repair on cables	29	0	0	0	0	0	0	86	0
<b>Sum</b>	<b>530</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>1856</b>	<b>1392</b>	<b>134</b>	<b>0</b>

Corrective Maintenance (unscheduled)									
Maintenance category	Vessel time requirement (Hour)					Crew time requirement (Hour)			
	CTVs	Crane vessels	Jack-up vessels	Helicopters	Daughter ships	On. Tur	Foundation	Electrical	Off. Tur
Cat. C1: Repair on turbines	4516	0	0	0	0	8164	0	0	0
Cat. C2: Replacement of minor parts (<2000kg)	0	144	0	0	0	546	0	0	0
Cat. C3: Replacement of major parts (>2000kg)	0	0	556	0	0	2687	0	0	0
Cat. C4: Repair/replacement on substations	6	0	0	0	0	0	0	15	0
Cat. C5: Repair/replacement of cables	7	0	0	0	0	0	0	20	0
<b>Sum</b>	<b>4529</b>	<b>144</b>	<b>556</b>	<b>0</b>	<b>0</b>	<b>11397</b>	<b>0</b>	<b>35</b>	<b>0</b>

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Figure 5: Requirement of vessel and personnel time

The optimised costs, including vessel, personnel and downtime costs, are illustrated in the cost estimation form (shown in Figure 6). Fixed and variable costs are considered in chartering a vessel, as well as other expenditures such as fuel consumption. Personnel cost is assumed to be an annual salary for each type of technician. The downtime cost is computed by the potential energy production during the breakdown and the wholesale electricity price. The DSS is able to provide an optimised O&M cost with different selected vessels and personnel; and it assists the project stakeholders to decide on the most suitable maintenance strategy.

It is not easy to investigate the ratios of vessel fixed cost and personnel cost between preventive and corrective works since they represent a single payment for each vessel or technician that is shared by both preventive and corrective maintenance. But the vessel variable cost should be proportional to the preventive and corrective workloads. As demonstrated by the results shown in Figure 6, the vessel variable cost spent on corrective maintenance is significantly higher than that of preventive maintenance. The downtime cost is broken down by separating the total amount into different maintenance categories. Corrective maintenance on wind turbines contributes a significant percentage (83%) of the



cost due to turbine breakdown. Such a high percentage could result from the higher frequency of corrective activities, and the longer replacement and logistics times.

Estimated Vessel Cost (£1,000,000)

Vessel type	The no. required	Fixed cost	Preventive maintenance		Corrective maintenance	
			Hours	Variable cost	Hours	Variable cost
Crew transfer vessels	3	0.548	530	0.016	4529	0.136
Crane vessels	1	0.090	0	0	144	0.288
Jack-up vessels	2	0.204	0	0	556	0.890
Helicopters	0	0	0	0	0	0
Daughter ships	0	N/A	0	0	0	0
Mother ships	0	0	N/A	N/A	N/A	N/A
Sum		0.842	530	0.016	5229	1.314

Estimated Personnel Cost (£1,000,000)

Personnel type	The no. required	Working hours	Personnel cost
Turbine technicians (onshore)	8	4876	0.384
Foundation technicians	3	2100	0.135
Electrical technicians	3	332	0.144
Turbine technicians (offshore)	0	15117	0
Sum			0.663

Estimated Revenue Loss (£1,000,000)

	P1	P2	P3	P4	Sum	C1	C2	C3	C4	C5	Sum
Breakdown hours	5087	88	2543	145	7863	22375	3009	13452	28	36	38900
Revenue loss	0.332	0.006	0.166	0.010	0.514	1.459	0.196	0.877	0.002	0.002	2.536

Total cost

£ 5,885 ,000

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Exit

Figure 6: Maintenance cost estimation

In addition, the deterministic model has been implemented to find the optimal solution in the sample case. A comparison of the results between the deterministic and stochastic models is given on Table 4. The stochastic model suggests hiring one additional turbine technician than the deterministic model as it considers potentially higher wind turbine failure rates. For the same reason, one additional lease period of crew transfer vessel and jack-up vessel are required to meet the higher maintenance demand. As a corresponding result of greater amount of maintenance resources, all of the optimised costs from the stochastic model are higher than those for the deterministic model. With the larger number of turbine technicians, the personnel cost presents 8% higher than deterministic model. The vessel fixed and variable costs from the stochastic model demonstrate 51% and 19% increase, respectively. Taking into account the relatively minor difference of 8% in the downtime costs, there is a 15% aggregate gap between the total costs from the deterministic and stochastic optimisation models. The more accurate technical data of breakdown rates, the more correct requirement of maintenance resources can be determined.

Table 4: Comparison of results between the deterministic and stochastic models

	Deterministic model	Stochastic model
<b>Technicians</b>		
Turbine technician (onshore)	7	8
Foundation technician	3	3
Electrical Technician	3	3
Turbine technician (offshore)	0	0
<b>Vessels</b>		
Crew transfer vessel	2	3
Crane vessel	1	1
Jack-up vessel	1	2
Helicopter	0	0
Daughter ship	0	0
<b>Costs</b>		
Personnel cost (£1,000,000)	0.615	0.663
Vessel fixed cost (£1,000,000)	0.557	0.842
Vessel variable cost (£1,000,000)	1.122	1.330
Mother ship cost (£1,000,000)	0	0
Downtime cost (£1,000,000)	2.833	3.050
<b>Total cost (£1,000,000)</b>	<b>5.127</b>	<b>5.885</b>

### 5.3 Sensitivity analysis

A sensitivity analysis has been conducted to evaluate the impact of an increase in the number of wind turbines installed in an OWF on the number of vessels and technicians needed to meet the maintenance demand, and the corresponding total costs. Although economies of scale may suggest that a lower cost per turbine may be achievable. The failure rates of different components in an OWF are another key parameter to determine the maintenance workload and the related costs. Therefore, the solutions from the DSS were investigated by changing value of the component failure rates and the number of wind turbines, in order to investigate its sensitivity in different situations.

#### • The effect of failure rates

An investigation with respect to failure rates was implemented with a variety of changes in failure rates, increasing and decreasing by 25% and 50%, in order to test the sensitivity of required maintenance resources. The numbers of technicians and vessels required to carry maintenance works illustrate the corresponding changes (see Table 5). One additional turbine technician is needed to meet the maintenance requirement with every 25% increase in the failure rates. The numbers of foundation technicians and electrical technicians are stable regardless of the increased or decreased failure rates. The effects on electrical and foundation technicians are not that significant because of the relatively lower breakdown frequency in foundations, substations and cables. No mother ship and offshore-based technicians are considered to take the maintenance tasks, with the changing failure rates. Such a result could be resulted from the nature of failures on offshore wind turbines; and relatively higher cost of mother ship might be another reason. The number of crew transfer vessels demonstrates an increase pattern; and longer charter lease of crane vessel and jack-up vessel are also requested to satisfy the growing maintenance demands. No helicopter is scheduled to provide service in maintenance plan, although it was assumed as available maintenance resource. This could result from the relatively higher costs and restricted compatibility to maintenance categories on this transportation mode.

Table 5: The effect of the varying failure rates on personnel, vessel and costs

	<b>Decreased by 50%</b>	<b>Decreased by 25%</b>	<b>Base rate</b>	<b>Increased by 25%</b>	<b>Increased by 50%</b>
<b>Technicians</b>					
<i>Turbine technician (onshore)</i>	6	7	8	10	11
<i>Foundation technician</i>	3	3	3	3	3
<i>Electrical Technician</i>	3	3	3	3	3
<i>Turbine technician (offshore)</i>	0	0	0	0	0
<b>Vessels</b>					
<i>Crew transfer vessel</i>	2	2	3	3	4
<i>Crane vessel</i>	1	1	1	1	2
<i>Jack-up vessel</i>	1	2	2	2	2
<i>Helicopter</i>	0	0	0	0	0
<i>Daughter ship</i>	0	0	0	0	0

As show on Figure 7, with the increased failure frequency by 25%, the personnel cost increases by 8-14% and vessel costs increase by 15-35%. The increase in downtime cost is more significant, 20-35%, compared to the investment on vessel and personnel. The downtime costs contribute more than 50% of the total costs in all the scenarios. In addition, the increase results in 18-31% aggregate growth in overall maintenance cost, as show by Figure 8.



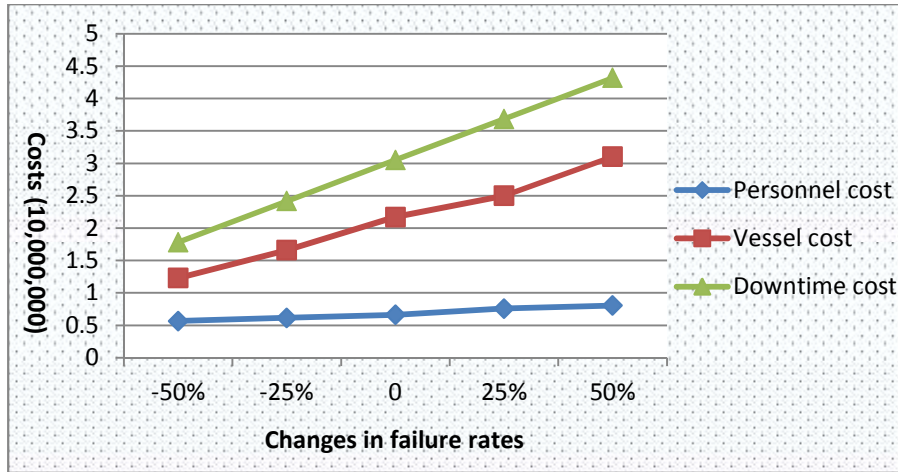


Figure 7: The effect of the failure rates on personnel, vessel and downtime costs

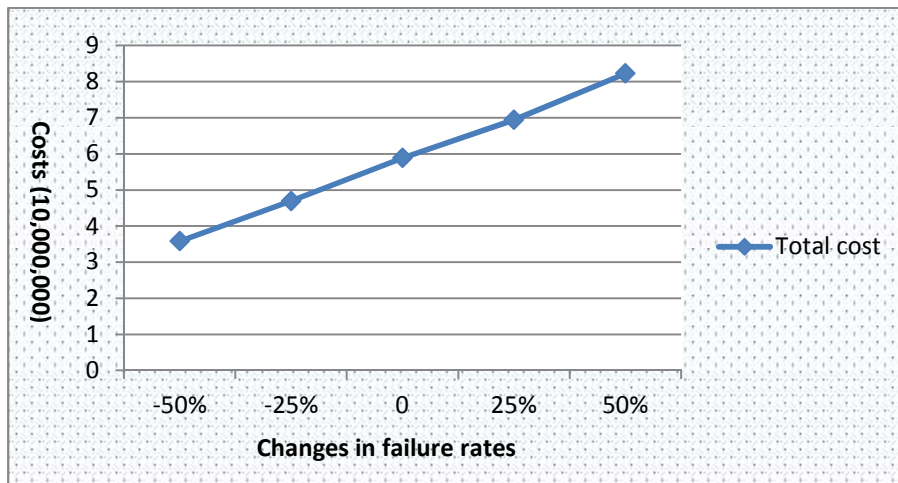


Figure 8: The effect of the failure rates on total cost

### ***The effect of the number of wind turbines***

The effect on the total optimised costs given by the DSS was also investigated by varying the number of wind turbines. Such sensitivity test is used to determine whether the DSS is suitable to a variety of offshore wind farms with different sizes, and to observe the variance in the required maintenance resources. Nine scenarios considering, 100, 125 ... 300 wind turbines, have been used to acquire the optimal solutions from the DSS. The stochastic decision making model was selected to implement this sensitivity analysis.

All costs including personnel, vessel and downtime present a near-linear increase, as shown on Figure 9. Since the personnel cost is contributed to by hiring maintenance technicians; it is observed that there is no significant variance by varying the number of wind turbines. The largest increase of personnel cost responding to 25 additional wind turbines is 15%, which was found between 100 and 125 turbines; and the smallest increase is 4% between 250 and 275 turbines. The variance of the vessel cost is observed from 6% to 26% with each increment of 25 wind turbines. The downtime cost is also affected; the maximum increase is 25% that is given between 100 and 125 turbines. The change of total maintenance costs is also demonstrated by a similar shape on Figure 10, which increases from 5.05 to 14.1 million with the growing size of the OWF.

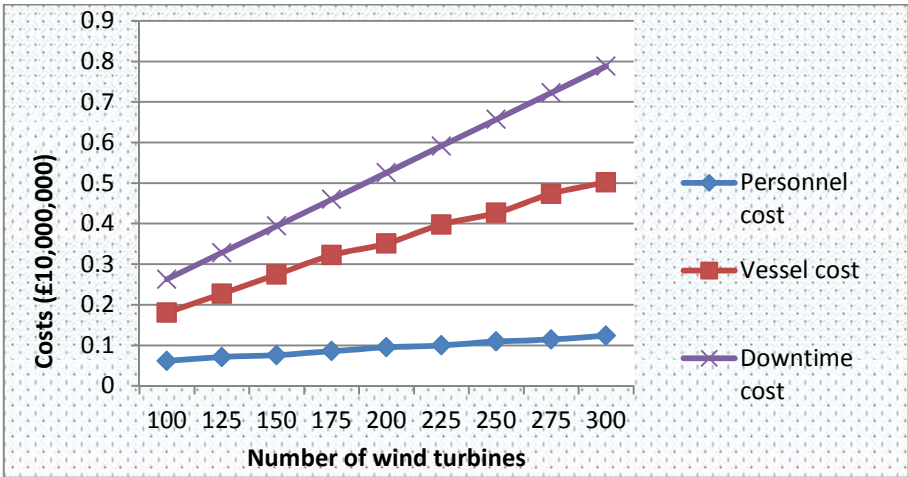


Figure 9: The effect of the number of wind turbines on personnel, vessel and downtime costs

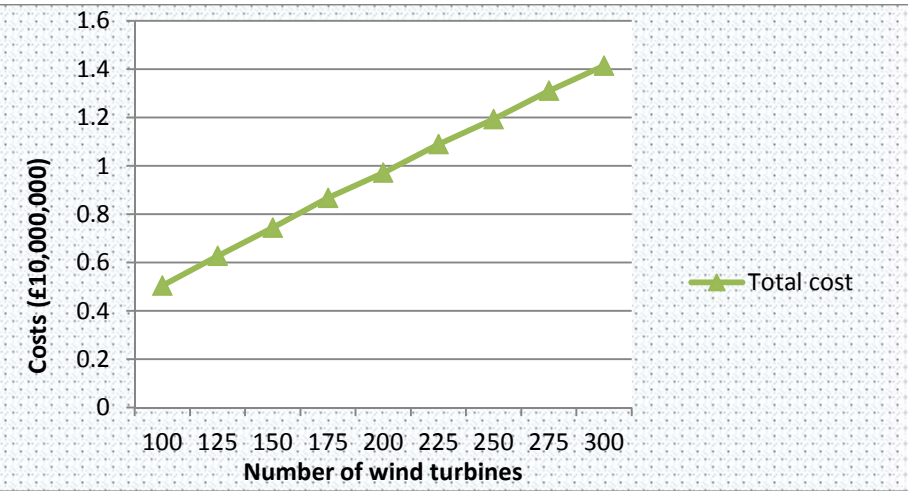


Figure 10: The effect of the number of wind turbines on total cost

#### 5.4 Comparison and validation of the performance of the proposed model using the case study of Dinwoodie et al. (2015)

This section evaluates and compares the performance of the proposed model to the results of the models published by Dinwoodie et al. (2015) using their case studies. As the deterministic model supplies more accurate results, which is more comparable with other model results. In the paper, a set of reference cases have been used to verify four decision support or simulation models: Strathclyde analysis tool, NOWIcob decision support tool, University of Stavanger (UiS) Simulation model and ECUME model. A base case consists of 80 wind turbines with the rated capacity of 3.0 MW, which is located 50km from an onshore maintenance base. Cables, substations and foundations in the wind farm were not considered for O&M operations in the offshore wind farm. Three vessel types were considered to carry out the annual services and five categories of corrective maintenance,

including manual resets, minor repair, medium repair, major repair and major replacement. There are three crew transfer vessels (CTV), one field support vessel (FSV), and one heavy-lift vessel (HLV) available in the base case. As no offshore based platform is involved in the maintenance strategy, onshore-based turbine technicians only are considered to take part in all the O&M activities. In addition, spare parts logistics are neglected for simplicity in order to carry out the comparison with the different models.

A comparison of results of the proposed deterministic model and the models in the literature is presented in Table 6. In the base case, all the cost results with the particular number of CTVs and technicians from the proposed model in the DSS are allocated within the result ranges published in the paper. The DSS model provided the maximal annual loss of production £21.54 million against other models, with an assumption of keeping 100% productivity under a desirable environment. Vessel cost is lower than other model results but repair cost stays at the highest level. In aggregate, therefore, direct O&M cost of the DSS model (£16.83 million) is just higher than the ECUME model but below three models.

Table 6: Results for the base case

	<b>DSS Model</b>	<b>Strathclyde CDT</b>	<b>NOWIcob</b>	<b>UiS Sim Model</b>	<b>ECUME model</b>	<b>Average</b>
Annual loss of production	£21.54 m	£17.28 m	£16.63 m	£15.48 m	£18.64 m	£17.91 m
Annual direct O&M cost	£16.83 m	£22.44 m	£25.17 m	£17.93 m	£14.48 m	£19.37 m
Annual vessel cost	£10.73 m	£17.84 m	£19.18 m	£12.24 m	£9.30 m	£13.86 m
Annual repair cost	£4.50 m	£3.00 m	£4.39 m	£4.08 m	£3.58 m	£3.91 m
Annual technician cost	£1.60 m	£1.60 m	£1.60 m	£1.60 m	£1.60 m	£1.60 m

The base case is implemented first, and then a number of other cases are generated from the base case for investigating the quantitative sensitivity, such as more (5) CTVs and fewer (1) CTVs, more (30) and fewer (10) technicians, failure rates down (50%) and up (200%). Figure 11 shows direct O&M costs for the base case and other cases. By comparing with the results of the other four models presented on the paper (Dinwoodie *et al.*, 2015), the quantitative trend is relatively consistent across the reference cases. The DSS results provide relative lower direct O&M costs in most of the reference cases, especially the almost minimal O&M cost in the case of more CTVs. Only the case of failure rates up affects the direct O&M cost on the DSS model more significantly than the other models.

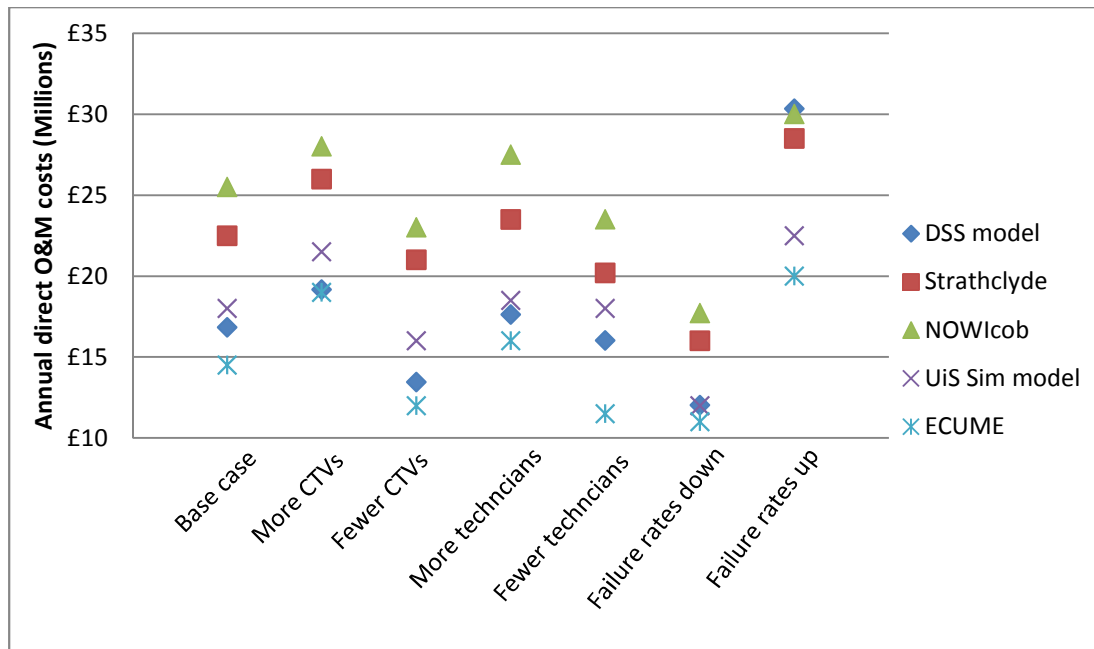


Figure 11: Annual direct O&M cost of the models for the reference cases

In addition, it is investigated to compare the annual direct O&M costs between optimal number of CTVs from DSS and other models applied in the related reference cases. The optimal solution to achieve the minimised total cost suggests that five CTVs, one FSV and one HLV are used to cover the maintenance requirement within the base case. It gives the same number of CTVs as the reference case of more CTVs, but the overall cost in the DSS optimal solution almost reaches the lowest boundary of result range of other four models. A similar investigation was carried out to compare the cost performance of the optimal number of technicians with other models. The DSS solution suggests that eleven technicians should be involved in maintenance activities and the corresponding annual O&M cost is located nearby the mid-point of the result range in the case of fewer technicians.

## 6. Conclusion and future work

### 6.1 Conclusion

As offshore wind is a relatively new technology, and there are a limited number of tools available to support O&M planning activities, a decision support system has been designed in this paper to assist multiple stakeholders in designing cost effective O&M decisions. The system proposed includes two optimisation models to minimise the total cost of O&M activities, including personnel cost, fixed vessel cost, variable vessel cost, mother ship cost and revenue loss, in offshore wind maintenance during a given period of time.

According to the results obtained from the DSS, offshore wind project developers can prepare O&M resources and organise works in advance to meet the requirement of necessary maintenance activities. All required maintenance resources will be used in a cost effective way in order to optimise the costing performance; and the revenue loss is seen as

another key element in O&M cost. Additionally, the costs are significantly affected by the reliability of offshore wind turbines and the size of the farm.

The implementation results imply that the reliability of OWF components has an immediate effect on the maintenance costs, as the majority of the costs are generated by corrective maintenance. Hence, the stochastic programming model (described in Section 4.2) is able to supply more realistic solutions if failure rates parameters are not known with certainty, since it takes into account a probabilistic failure rates for each OWF component. Such probabilistic data is critical to determine the unforeseen requirement of vessels and technicians for corrective maintenance, in order to maximise the availability of energy production. The stochastic model is thus aimed at OWF stakeholders who do not have significant certainty about turbine failure rates due to lack of knowledge. On the other hand, the deterministic model could be used by OWF stakeholders who are in the position to make more accurate conclusions about the failure rates due to their industrial knowledge. Thus the 15% gap in total costs between the deterministic and stochastic models can be seen as a proxy to the value of information regarding turbine failure rates. The DSS also gives an opportunity to understand the sensitivities of the O&M costs due to changes in failure probability and OWF size. The sensitivity results illustrate near-linear changes in O&M costs by varying the failure rates and the number of turbines. Hence, the DSS is able to help offshore wind stakeholders to understand the strategic resource requirements associated with the maintenance of an offshore wind farm. Utilisation of vessels and technicians could potentially be included as further objectives in the optimisation models. In addition, the correlation between preventive maintenance and component failures could be an extra parameter to consider in the further research.

## ***6.2 Future work on the incorporation of weather conditions***

The effect of weather is one of the most significant factors causing uncertainty in the planning of offshore wind farms. Currently, weather is only accurately predictable on a timescale far shorter than the strategic planning periods considered by the models developed in this paper. The usage examples given in Sections 4 and 5 have been populated by using long-term average weather data from the United Kingdom. However, it is recognised that weather conditions different from the average will result in a performance significantly different from that predicted by the model. The suggested course of action for stakeholders that are concerned by the variance is therefore to execute the model for multiple weather scenarios with different input data in each scenario. The optimal course(s) of action could then be determined by a technique such as discrete news-vendor analysis, which allows for either probabilistic or non-probabilistic analysis, dependent on whether the stakeholder wishes to assign probabilities to the chances of a weather scenario occurring or not.

Calculation of the effects of a given weather scenario on the input data of the models presented in Section 4 requires a significant level of understanding of offshore wind operations. As well as the obvious restrictions on accessibility of platforms, the weather will have an effect on the vessel travel times and potentially the vessel availability and charter costs as a poor weather season may induce increased demand for vessels in the smaller time periods of adequate weather conditions. There may also be some effect on the failure rates as harsher than average weather may cause a larger number of failures. The effect on personnel should also not be neglected as seasickness and more challenging working conditions could reduce the number of working hours, number of available technicians in each category and the number of available working days per technician per year. The above paragraph states the considerations in the negative “worse weather than average” scenarios; however the same reasoning also applies in reverse to the positive “better weather than

average” scenarios. It is recognised that accurate compilation of the above data for multiple weather scenarios will only be possible for stakeholders with knowledge of and access to wind farm operations data. Therefore it is suggested that, similar to the failure rate case detailed in Section 4, two options for usage of the models are available. Stakeholders without access to detailed weather effect data may use the models as presented with solely the average case to gain an estimate of costs and resources, with the caveat that weather conditions significantly different to the average will results in significantly different resource and cost levels. Stakeholders with access to detailed operational data are recommended to use the approach outlined in the above paragraphs, forming multiple weather data effect scenarios and making decisions, possibly with use of a further analysis technique, based on the model results from across the set of weather data effect scenarios.

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## References

- Agilent Technologies (2007). VBA Programmer's Guild, 4<sup>th</sup> Edition.
- Appiott J, Dhanju A and Cicin- Sain B (2014). Encouraging renewable energy in the offshore environment. *Ocean & Coastal Management* 90: 58-64.
- Beerbuhl SS, Frohling M and Schultmann (2015). Combined scheduling and capacity planning of electricity-based ammonia production to integrate renewable energies. *European Journal of Operational Research* 241: 851-862.
- Besnard F, Fischer K and Tjernberg L B (2013). A model for the optimisation of the maintenance support organisation for offshore wind farms. *IEEE Transactions on Sustainable Energy* 4(2): 443-450
- Bilgili M, Yasar A and Simsek E (2011). Offshore wind power development in Europe and its comparison with onshore counterpart. *Renewable and Sustainable Energy Reviews* 15(2): 905-915.
- Breton S and Moe G (2009). Status, plans and technologies for offshore wind turbines in Europe and North America. *Renewable Energy* 34(3): 646-654.
- Bussel G J W V and Schontag C (1997). Operation and maintenance aspects of large offshore wind farms.
- Carbon Trust (2008). Offshore wind power: big challenge, big opportunity. Online <http://www.carbontrust.com/media/42162/ctc743-offshore-wind-power.pdf>
- Chang K H (2014). A decision support system for planning and coordination of hybrid renewable energy systems. *Decision Support Systems* 64: 4-13.
- Connolly D, Lund H, Mathiesen B and Leahy M (2010). A review of computer tools for analysing the integration of renewable energy into various energy systems. *Applied Energy* 874: 1059-1082.
- Dai L, Ehlers S, Rausand M and Utne IB (2013). Risk of collision between service vessels and offshore wind turbines. *Reliability Engineering and System Safety* 109: 18-31.
- Dalgic Y, Lazakis I and Turan O (2013). Vessel charter rate estimation for offshore wind O&M activities. *Developments in Maritime Transportation and Exploitation of Sea Resources*, Print ISBN: 978-1-138-00124-4, Chapter 99: 899-907.
- Dekker R, Bloemhof J and Mallidis I (2012). Operations research for green logistics – An overview of aspects, issues, contributions and challenges. *European Journal of Operational Research* 219: 671-679.
- Ding F and Tian Z (2012). Opportunistic maintenance for wind farms considering multi-level imperfect maintenance thresholds. *Renewable Energy* 45: 175-182.
- Dinwoodie I, McMillan D, Revie M, Lazakis I, Dalgic Y (2013). Development of a combined operational and strategic decision support model for offshore wind. *Energy Procedia* 35: 157-166.



1062 Dinwoodie I, Endrerud OE V, Hofmann M, Martin R, Sperstad I B (2015). Reference cases  
1063 for verification of offshore O&M simulation models for offshore wind farms. *Wind Engineering*  
1064 39: 1-14.

1065 European Wind Energy Association (2009). Wind energy – the fact: a guide to the  
1066 technology, economics and future of wind power. London, UK. Online  
1067 <http://www.goodreads.com/book/show/6381844-wind-energy---the-facts>

1068 Friris L and Infield D (2009). *Renewable energy: in power systems*. Chichester: John Wiley  
1069 and Son Limited, Print ISBN: 978-0-470-01749-4.

1070 Gao X, Yang H and Lu L (2014). Study on offshore wind power potential and wind farm  
1071 optimisation in Hong Kong. *Applied Energy* 130: 519-531.

1072 Hameed Z, Vatn J and Heggset J (2011). Challenges in the reliability and maintainability  
1073 data collection for offshore wind turbines. *Renewable Energy* 36: 2154-2165.

1074 Halvorsen-Weare E E, Gundegjerde C, Halvoesen IB, Hvattum LM and Nonas L M (2013).  
1075 Vessel fleet analysis for maintenance operations at offshore wind farms. *Energy Procedia* 35:  
1076 167-176.

1077 Higgins P and Foley A (2014). The evolution of offshore wind power in the United Kingdom.  
1078 *Renewable and Sustainable Energy Reviews* 37: 599-612.

1079 Hunt J D, Banares-Alcantara R and Hanbury D (2013). A new integrated tool for complex  
1080 decision making: Application to the UK energy sector. *Decision Support Systems* 54: 1427-  
1081 1441.

1082 Krokoszinski HJ (2003). Efficiency and effectiveness of wind farms – keys to cost optimised  
1083 operation and maintenance. *Renewable Energy* 28: 2165-2178.

1084 Laura C S and Vicente D C (2014). Life-cycle cost analysis of floating offshore wind farms.  
1085 *Renewable Energy* 66: 41-48.

1086 Li X, Ouelhadj D, Song X, Jones D, Wall G, Howell K E, Igwe P, Martin S, Song D and Pertin  
1087 E (2015a). WP1report: Maintenance Decision Support Tool, *2OM Project*.  
1088

1089 Li X, Ouelhadj D, Song X, Jones D, Wall G, Howell K E, Igwe P, Martin S, Song D and Pertin  
1090 E (2015b). WP4 report: Communication, *2OM Project*.  
1091

1092 Michler-Cieluch T, Krause G and Buck BH (2009). Reflections on integrating operation and  
1093 maintenance activities of offshore wind farms and mariculture. *Ocean & Coastal*  
1094 *Management* 52: 57-68.

1095 Minguez R, Martinez M, Castellanos OF and Guanche R (2011). Component failure  
1096 simulation tool for optimal electrical configuration and repair strategy of offshore wind farms.  
1097 In: *OCEANS, 2011 IEEE*, Spain: 1-10.

1098 Mirzapour Al-e-hashem S M J, Baboli A and Sazvar Z (2013). A stochastic aggregate  
1099 production planning model in a green supply chain: considering flexible lead times, nonlinear  
1100 purchase and shortage cost functions. *European Journal of Operational Research* 230: 26-  
1101 41.

1102 Most D and Keles D (2010). A survey of stochastic modelling approaches for liberalised  
1103 electricity markets. *European Journal of Operational Research* 207: 543-556.



- 1104 Mostafaeipour A (2010). Feasibility study of offshore wind turbine installation in Iran  
1105 compared with world. *Renewable and Sustainable Energy Reviews* 14(7): 1722-1743.
- 1106 Myhr A, Bjerkseter C, Agotnes A and Nygaard TA (2014). Levelised cost of energy for  
1107 offshore floating wind turbines in a life cycle perspective. *Renewable Energy* 66: 714-728.
- 1108 Nielsen JJ and Sorensen JD (2011). On risk-based operation and maintenance of offshore  
1109 wind turbine components. *Reliability Engineering and System Safety* 96: 218-229.
- 1110 Ochieng EG, Melaine Y, Potts SJ, Zuofa T, Egbu CO, Price ADF and Ruan X (2014). Future  
1111 for offshore wind energy in the United Kingdom: The way forward. *Renewable and  
1112 Sustainable Energy Reviews* 39: 655-666.
- 1113 O'Keeffe A and Haggett C (2012). An investigation into the potential barriers facing the  
1114 development of offshore wind energy in Scotland: Case study – Firth of Forth offshore wind  
1115 farm. *Renewable and Sustainable Energy Reviews* 16: 3711-3721.
- 1116 Pahlke T (2007). Software & Decision Support Systems for Offshore Wind Energy  
1117 Exploitation in North Sea Region. In: *Pushing Offshore Wind Energy Regions EU*: 1-10.  
1118 Online [http://pcoe.nl/@api/deki/files/1900/=12wp1\\_executivesummary\\_sdss-studie\\_2007-  
1119 06-05.pdf](http://pcoe.nl/@api/deki/files/1900/=12wp1_executivesummary_sdss-studie_2007-06-05.pdf)
- 1120 Perez B, Minguez R and Guanche (2013). Offshore wind farm layout optimisation using  
1121 mathematical programming techniques. *Renewable Energy* 53: 389-399.
- 1122 Prassler T and Schaechtele J (2012). Comparison of the financial attractiveness among  
1123 prospective offshore wind parks in selected European countries. *Energy Policy* 45(6): 86-101.
- 1124 Rademakers LWMM, Braam H, Zaaier MB and Van Bussel GJW (2003). Assessment and  
1125 optimisation of operation and maintenance of offshore wind turbines. In: *Proceedings of the  
1126 European Wind Energy Conference (EWEC)*, Madrid, Spain.
- 1127 Scheu M, Matha D, Hofmann M and Muskulus M (2012). Maintenance strategies for large  
1128 offshore wind farms. *Energy Procedia* 24: 281-288.
- 1129 The Crown Estate (2010). A guide to an offshore wind farm. Online  
1130 [http://www.thecrownestate.co.uk/media/5408/ei-km-in-sc-supply-012010-a-guide-to-an-  
1131 offshore-wind-farm.pdf](http://www.thecrownestate.co.uk/media/5408/ei-km-in-sc-supply-012010-a-guide-to-an-offshore-wind-farm.pdf)
- 1132 Wagner HJ, Baack C, Eickelkamp T, Epe A, Lohmann J and Troy S (2011). Life cycle  
1133 assessment of the offshore wind farm Alpha Ventus. *Energy* 36: 2459-2464.
- 1134 Wanderer T (2009). *Development of a GIS Based Decision Support System for Offshore  
1135 Wind Energy use in the North Sea*. Diploma Thesis. Ludwig-Maximilians-University, Munich.
- 1136 Wang Z, Jiang C, Qian A and Wang C (2009). The key technology of offshore wind farm and  
1137 its new development in China. *Renewable and Sustainable Energy Reviews* 13(1): 216-222.
- 1138 Willis K O and Jones D F (2008). Multi-objective simulation optimisation through search  
1139 heuristics and relational database analysis. *Decision Support Systems* 48: 277-286.
- 1140 Van de Pieterman RP, Braam H, Obdam TS, Rademakers LWMM, Van der Zee TJJ (2011).  
1141 Optimisation of maintenance strategies for offshore wind farms: A case study performed with  
1142 the OMCE-Calculator. *Present at: The offshore 2011 conference, Amsterdam, The  
1143 Netherlands*.
- 1144  
1145 Zhang Z, Kusiak A and Song Z (2013). Scheduling electric power production at a wind farm.  
1146 *European Journal of Operational Research* 224: 227-238.